

3.)

$$\dot{W}_{\text{cycle}} = \dot{Q}_1 - \dot{Q}_2$$

$$\Rightarrow 40 = \dot{Q}_1 - \frac{1000}{60}$$

$$\Rightarrow \dot{Q}_1 = 56.67 \text{ kW}$$

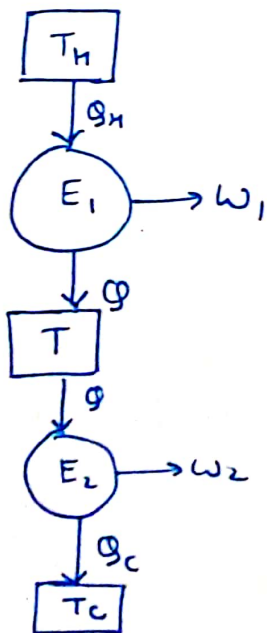
For a reversible cycle, $\frac{\dot{Q}_1}{\dot{Q}_2} = \frac{T_1}{T_2} \Rightarrow \frac{56.67}{1000} = \frac{T_1}{200}$

~~$\Rightarrow T_1 = 1133.4 \text{ K}$~~

$$\frac{56.67}{1000} \times 60 = \frac{T_1}{T_2} = \frac{T_1}{200}$$

$$\Rightarrow T_1 = 680.04 \text{ K}$$

6.)



(a) net work of 2 cycles are equal.

$$\therefore W_1 = W_2$$

$$\Rightarrow Q_h - Q = Q - Q_c$$

$$\Rightarrow \frac{Q_h}{Q} - 1 = 1 - \frac{Q_c}{Q} \Rightarrow \frac{T_h}{T} - 1 = 1 - \frac{T_c}{T}$$

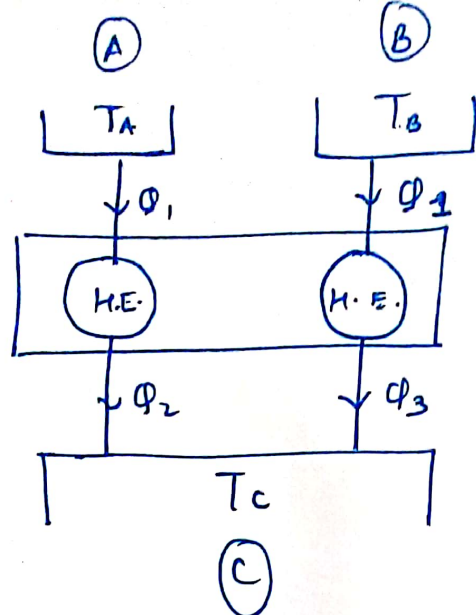
$$\Rightarrow \frac{T_h + T_c}{T} = 2 \Rightarrow T = \frac{T_h + T_c}{2}$$

(b) thermal efficiencies of the 2 cycles are equal.

$$\eta_1 = \eta_2 \Rightarrow 1 - \frac{Q}{Q_h} = 1 - \frac{Q_c}{Q}$$

$$\Rightarrow \frac{Q}{Q_h} = \frac{Q_c}{Q} \Rightarrow \frac{T}{T_h} = \frac{T_c}{T} \Rightarrow T = \sqrt{T_c T_h}$$

9.)



η of heat engine between (A) & (C)

$$\eta_A = 1 - \frac{T_C}{T_A}$$

$$\therefore \eta \text{ of our engine} = \alpha \left(1 - \frac{T_C}{T_A} \right) \quad - (1)$$

For our engine,

$$\text{Total heat addition} = 2Q_1 \quad - (2)$$

$$\text{Total heat rejection} = Q_2 + Q_3 \quad - (3)$$

$$\frac{Q_2}{Q_1} = \frac{T_C}{T_A} \Rightarrow Q_2 = Q_1 \frac{T_C}{T_A} \quad - (4)$$

$$\frac{Q_3}{Q_1} = \frac{T_C}{T_B} \Rightarrow Q_3 = Q_1 \frac{T_C}{T_B} \quad - (5)$$

Substitute (5) & (4) in (3),

$$\therefore \text{Total heat rejection} = Q_2 + Q_3 = Q_1 T_C \left(\frac{1}{T_A} + \frac{1}{T_B} \right) \quad - (6)$$

Using (2) & (6),

$$\begin{aligned} \eta \text{ of our engine} &= 1 - \frac{Q_2 + Q_3}{2Q_1} \\ &= 1 - \frac{Q_1 T_C \left(\frac{1}{T_A} + \frac{1}{T_B} \right)}{2Q_1} \\ &= 1 - \frac{T_C}{2} \left(\frac{1}{T_A} + \frac{1}{T_B} \right) \quad - (7) \end{aligned}$$

Equation ① & ⑦,

$$\alpha \left(1 - \frac{T_C}{T_A} \right) = 1 - \frac{T_C}{2} \left(\frac{1}{T_A} + \frac{1}{T_B} \right)$$

Multiply both sides by $\frac{T_A}{T_C}$,

$$\alpha \frac{T_A}{T_C} - \alpha = \frac{T_A}{T_C} - \frac{1}{2} - \frac{1}{2} \frac{T_A}{T_B}$$

$$\begin{aligned} \therefore \frac{T_A}{2T_B} &= \cancel{\left(\frac{1}{2} - \alpha \right)} \quad \alpha - \frac{1}{2} + \frac{T_A}{T_C} - \alpha \frac{T_A}{T_C} \\ &= \left(\alpha - \frac{1}{2} \right) + \frac{T_A}{T_C} (1 - \alpha) \end{aligned}$$

$$\therefore \frac{T_A}{T_B} = (2\alpha - 1) + 2(1 - \alpha) \frac{T_A}{T_C}$$

2.) Maximum efficiency = $1 - \frac{T_2}{T_1}$

$$= 1 - \frac{400}{800} = 0.5$$

$$\begin{aligned} \therefore \text{Maximum work output} &= 0.5 \times 105 \text{ MJ} \\ &= 52.5 \text{ MJ} \end{aligned}$$

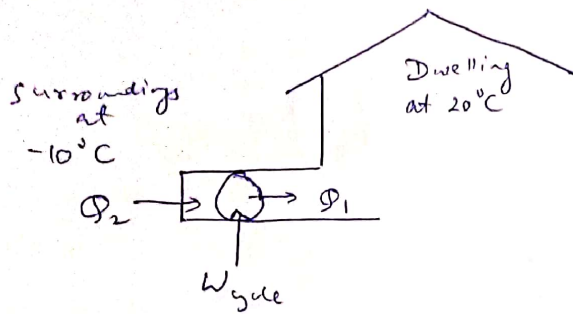
Claim of work, $W = 17.5 \text{ kWh}$

$$= 17.5 \times 10^3 \times 3600 \text{ J}$$

$$= 63 \text{ MJ} > 52.5 \text{ MJ}$$

So, one should not invest money to put his engine in the market.

5.)



Heat Pump must provide 3.5×10^6 kJ per day to a dwelling to maintain its temperature at 20°C .

Electricity cost $\rightarrow$ Rs 5.0 per kWh

$$\text{COP}_{\text{max}} = \frac{T_1}{T_1 - T_2} = \frac{293}{293 - 263} = 9.77$$

$$\therefore \dot{W}_{\text{min}} = \frac{\dot{Q}_1}{\text{COP}} = \frac{3.5 \times 10^6 \text{ kJ}}{9.77} = 0.358 \times 10^6 \text{ kJ per day}$$

$$1 \text{ kWh} = 3.6 \times 10^6 \text{ J}$$

$$\therefore 0.358 \times 10^6 \text{ kJ} = 0.358 \times 10^9 \text{ J} = \frac{0.358 \times 10^9}{3.6 \times 10^6} \text{ kWh} = 99.44 \text{ kWh}$$

$$\therefore \text{In one day, theoretical total operating cost} = 99.44 \text{ kWh} \times \text{Rs } 5.0 \text{ per kWh} = \text{Rs } 497.22$$

8.)

Refrigeration cycle - $\text{COP} = 3$

Maintains a computer lab at $18^\circ\text{C} = 291 \text{ K}$ on a day when the outside temperature is $30^\circ\text{C} = 303 \text{ K}$.

$$\begin{aligned} \text{Thermal load} &= 30000 \frac{\text{kJ}}{\text{hr}} + 6000 \frac{\text{kJ}}{\text{hr}} \\ &= 36000 \frac{\text{kJ}}{\text{hr}} = \frac{36000 \text{ kJ}}{3600 \frac{\text{s}}{\text{hr}}} \\ &= 10 \text{ kW} \end{aligned}$$

$$W = \frac{Q_c}{\text{COP}} = \frac{10 \text{ kW}}{3} = 3.33 \text{ kW}$$

In case of a reversible refrigerator, COP can be ~~also~~ calculated using the absolute hot and cold temperatures.

$$\text{COP}_{\text{rev}} = \frac{1}{\frac{T}{T_c} - 1} = \frac{1}{\frac{303}{241} - 1}$$
$$= 24.25$$

For the same thermal load, the minimum theoretical power required = power required by a reversible cycle

$$= \frac{Q_c}{\text{COP}} = \frac{10 \text{ kW}}{24.25} = 0.4124 \text{ kW}$$

1.) Given

$$\dot{Q}_2 = 8000 \text{ kJ/hr}$$

$$\text{COP} = 8.5$$

$$\dot{W} = \frac{\dot{Q}_2}{\text{COP}} = \frac{8000}{8.5} = 941.18 \text{ kJ/hr}$$

For a reversible cycle

$$\text{COP}_{\text{rev}} = \frac{T_2}{T_1 - T_2} = \frac{273 + 0}{293 - 273} = 13.65$$

$$\Rightarrow \dot{W}_{\text{rev}} = \frac{\dot{Q}_2}{13.65} = \frac{8000}{13.65} = 586.1 \text{ kJ/hr}$$

which is $5\frac{1}{2}$ times less.

4.)

Given, $\eta = 0.29$

required ratio = $\frac{\text{heat transfer to radiator}}{\text{heat transfer to heat engine}}$

$$= \frac{Q_c' + Q_H'}{Q_H'}$$

By first law,

$$Q_H - Q_c' = W = Q_H' - Q_c \quad (\text{HP})$$

$$\eta = 1 - \frac{Q_c'}{Q_H}$$

$$= 0.29$$

(definition for heat engine)

$$\frac{Q_c'}{Q_H} = 0.71$$

$$\text{COP} = 3.5$$

$$= \frac{Q'_H}{Q'_H - Q_C}$$

(definition for heat pump)

$$\Rightarrow 1 - \frac{Q_C}{Q'_H} = \frac{1}{3.5} = 0.2857$$

$$\frac{Q_C}{Q'_H} = 0.7143$$

Plugging in first law,

$$0.29 Q_H = Q'_H - Q_C \Rightarrow 0.29 \frac{Q_H}{Q'_H} = 1 - \frac{Q_C}{Q'_H}$$

$$\Rightarrow \frac{Q'_H}{Q_H} = 1.015$$

$$\text{Therefore required ratio} = \frac{Q'_C}{Q_H} + \frac{Q'_H}{Q_H} = 0.7143 + 1.015 = \underline{\underline{1.725}}$$

7))

Given,

$$m_A = 20 \text{ kg}$$

$$m_B = 10 \text{ kg}$$

$$T_A = 1000 \text{ K}$$

$$T_B = 300 \text{ K}$$

$$W_{\max} ? \quad T_{\text{final}} = ?$$

Engine stops when $T_{Af}^* = T_{Bf}^* = T_f^*$

and maximum work $\Rightarrow$ reversible process

By first law

@ A

$$\delta Q_A - \delta W_A = dU_A$$

$$\Rightarrow \delta Q_A = dU_A = m_A C_v dT_A$$

@ B

$$\delta Q_B - \delta W_B = dU_B$$

$$\delta Q_B - p dV_B = dU_B \Rightarrow \delta Q_B = dU_B + p dV_B = dH_B \\ = m_B C_p dT_B$$

Reversible $\Rightarrow \frac{\delta Q_A}{T_A} = \frac{\delta Q_B}{T_B}$

$$\Rightarrow -m_A C_v \frac{dT_A}{T_A} = m_B C_p \frac{dT_B}{T_B}$$

because dT_A is -ve
and heat transfer to engine is positive

$$\Rightarrow \frac{-dT_A}{T_A} = 0.7 \frac{dT_B}{T_B}$$

On integration from respective lower limits to T_f

$$\int_{1000}^{T_f} \frac{-dT_A}{T_A} = 0.7 \int_{300}^{T_f} \frac{dT_B}{T_B}$$

$$-\ln(T_f/1000) = 0.7 \ln(T_f/300)$$

$$\Rightarrow T_f = 609.11 \text{ K.}$$

By first law

$$\delta W = \delta Q_A - \delta Q_B$$

$$= -m_A C_v dT_A - m_B C_p dT_B$$

$$= -20 \times 717.5 \times (609.11 - 1000) - 10 \times 1004.5 \times (609.11 - 300)$$

$$= \underline{\underline{2504.2615 \text{ kJ}}}$$